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## European Technical Assessment ETA-22/0089 of 2024/12/13

I General Part

Technical Assessment Body issuing the ETA and designated according to Article 29 of the Regulation (EU) No 305/2011: ETA-Danmark A/S

Trade name of the construction product:

Rotho Blaas NINO Angle Brackets and WKR Hold Downs

Product family to which the above construction product belongs:

Three-dimensional nailing plate (Angle Bracket or Hold Down for timber-to-timber or timber-to-concrete or steel connections)

Manufacturer:

ROTHO BLAAS SRL Via dell'Adige 2/1 IT-39040 Cortaccia (BZ) Tel. + 39 0471 818400 Fax + 39 0471 818484 Internet www.rothoblaas.com ROTHO BLAAS SRL Held on file by ETA-Danmark AS

Manufacturing plant:

35 pages including 2 annexes which form an integral part of the document

This European Technical Assessment contains:

EAD 130186-00-0603 for Three-dimensional nailing plates

This European Technical Assessment is issued in accordance with Regulation (EU) No 305/2011, on the basis of:

The ETA issued on 2022-08-25

This version replaces:

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#### II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

#### 1 Technical description of product

#### Technical description of the product

Rotho Blaas angle brackets and hold downs are one-piece non-welded, face-fixed angle brackets to be used in timber to timber or in timber to concrete or timber to steel connections. They are connected to construction members made of timber or wood-based products with threaded (ringed shank) type LBA nails according to ETA-22/0002 or ringed shank nails according to EN 14592 or screws type LBS or HBSPL according to ETA-11/0030 or screws type HBS with or without HUS washer according to ETA-11/0030 or screws type HBSP with WU2 washer head according to ETA-11/0030 or screws type TBS with large washer head according to ETA-11/0030 or screws type VGS with or without HUS washer according to ETA-11/0030 or bolts according to EN 14592 and to concrete or steel members with bolts or metal anchors.

The angle brackets and hold downs with a steel plate thickness of up to 3,5 mm are made from the following material:

- steel S235 / Z 275 or FeZn12c according to EN 10025:2005 with  $R_e \ge 235$  N/mm²,  $R_m \le 510$  N/mm² and  $A_{80} \ge 26\%$
- steel S355 / Z 275 or FeZn12c according to EN 10025:2005 with  $R_e \ge 355$  N/mm²,  $R_m \le 630$  N/mm² and  $A_{80} \ge 22\%$
- steel S275 / Z 275 or FeZn12c according to EN 10025:2005 with  $R_e \ge 275$  N/mm²,  $R_m \le 560$  N/mm² and  $A_{80} \ge 23\%$
- steel DX51D / Z 275 or FeZn12c according to EN 10346:2015 with  $R_e \ge 235$  N/mm²,  $R_m \le 500$  N/mm² and  $A_{80} \ge 22\%$
- steel S250GD / Z 275 according to EN 10346:2015 with  $R_e \ge 250$  N/mm²,  $R_m \! \le \! 470$  N/mm² and  $A_{80} \! \ge 19\%$
- steel S350GD / Z 275 according to EN 10346:2015 with  $R_e \geq 350$  N/mm²,  $R_m \geq 420$  N/mm² and  $A_{80} \geq 16\%$
- Stainless steel with  $R_e \ge 235 \text{ N/mm}^2$ ,  $R_m \le 630 \text{ N/mm}^2$  and  $A_{80} \ge 22\%$

Dimensions, hole positions and typical installations are shown in Annex B. Rotho Blaas angle brackets and hold downs are made from steel with tolerances according to EN 10143.

# 2 Specification of the intended use in accordance with the applicable European Assessment Document (hereinafter EAD)

The angle brackets and hold downs are intended for use in making connections in load bearing timber structures, as a connection between a beam and a purlin, or as a connection between wall and floor elements or as wall-to-wall connection and on concrete/steel elements, where requirements for mechanical resistance and stability and safety in use in the sense of the Basic Works Requirements 1 and 4 of Regulation (EU) 305/2011 shall be fulfilled.

The connection may be with a single angle bracket or hold down or with an angle bracket or hold down on each side of the fastened timber member (see Annex B).

The static and kinematical behaviour of the timber members or the supports shall be as described in Annex A and B

The wood members may be of solid timber, glued laminated timber and similar glued members, or wood-based structural members with a characteristic density from 290 kg/m³ to 420 kg/m³. The wood members may be of Laminated Veneer Lumber (LVL) with a characteristic density up to 500 kg/m³ with nails/screws in the wide face of the LVL component. This requirement to the material of the wood members can be fulfilled by using the following materials:

- Structural solid timber according to EN 14081,
- Glulam according to EN 14080 or ETA,
- Glued solid timber according to EN14080,
- LVL according to EN 14374 or ETA,
- Parallam PSL,
- Intrallam LSL,
- Cross laminated timber according to ETA,
- Plywood according to EN 636 or ETA,
- Engineered wood products with certified load-carrying capacities for connections with dowel-type fasteners.

Annex B states the load-carrying capacities of the angle bracket or hold down connections for a characteristic density of  $350 \text{ kg/m}^3$ . For timber or wood-based material with a lower or higher characteristic density than  $350 \text{ kg/m}^3$  the load-carrying capacities shall be converted by the factor  $k_{dens}$ :

In load case F<sub>1</sub>:

$$\begin{split} k_{dens}^{} = & \left(\frac{\rho_k}{350}\right)^{\!0.8} \text{ for } 290 \text{ kg/m}^3 \leq \rho_k \leq 350 \text{ kg/m}^3 \\ k_{dens}^{} = & 1 & \text{for } \rho_k > 350 \text{ kg/m}^3 \end{split}$$

In load case  $F_{2/3}$ ,  $F_4$  and  $F_{45}$  for timber materials except L.VI.:

$$k_{dens} = \left(\frac{\rho_k}{350}\right)^{0.5}$$
 for 290 kg/m<sup>3</sup>  $\leq \rho_k \leq 420$  kg/m<sup>3</sup>

In load case  $F_{2/3}$ ,  $F_4$  and  $F_{45}$  for LVL:

$$k_{dens} = \left(\frac{\rho_k}{350}\right)^{0.5} \text{ for LVL with } \rho_k \leq 500 \text{ kg/m}^3$$

where  $\rho_k$  is the characteristic density of the timber material in kg/m<sup>3</sup>.

If a wood-based panel, GFB or a soundproofing interlayer with a thickness of not more than 26 mm is placed between the connector plate and the timber member, the lateral load-carrying capacity of the nail or screw, respectively, has to take into account the effect of the interlayer.

The design of the connections shall be in accordance with Eurocode 5 or a similar national Timber Code. The wood members shall have a thickness which is larger than the penetration depth of the nails into the members.

The angle brackets and hold downs are primarily for use in timber structures subject to the dry, internal conditions defined by service classes 1 and 2 of Eurocode 5 and for connections subject to static or quasi-static loading. This includes seismic actions.

The angle brackets and hold downs can also be used in outdoor timber structures, service class 3, when a corrosion protection in accordance with Eurocode 5 is applied, or when stainless steel with similar or better characteristic yield strength and ultimate strength is employed.

The angle brackets and hold downs may also be used for connections between a timber member and a member of concrete or steel.

The scope of the angle brackets and hold downs regarding resistance to corrosion shall be defined according to national provisions that apply at the installation site considering environmental conditions and in conjunction with the admissible service conditions according to EN 1995-1-1 and the admissible corrosivity category as described and defined in EN ISO 12944-2.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the angle brackets and hold downs of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

## 3 Performance of the product and references to the methods used for its assessment

Characteristic	Assessment of characteristic	
3.1 Mechanical resistance and stability*) (BWR1)		
Joint Strength - Characteristic load-carrying capacity	See Annex B	
Joint Stiffness	See Annex B	
Joint ductility	No performance assessed	
Resistance to seismic actions	No performance assessed	
Resistance to corrosion and deterioration	See section 3.6	
3.2 Safety in case of fire (BWR2)		
Reaction to fire	The angle brackets and hold downs are made from steel classified as Euroclass A1 in accordance with EN 13501-1 and Commission Delegated Regulation 2016/364	
3.3 General aspects related to the performance of the product	The angle brackets and hold downs have been assessed as having satisfactory durability and serviceability when used in timber structures using the timber species described in Eurocode 5 and subject to the conditions defined by service class 1 and 2	
Identification	See Annex A	

<sup>\*)</sup> See additional information in section 3.4 - 3.7.

# 3.4 Methods of verification Safety principles and partial factors

The characteristic load-carrying capacities are based on the characteristic values of the dowel-type connections and the steel plates. To obtain design values the capacities must be divided by different partial factors for the material properties, in case of failure of connections between the angle bracket or hold down to a timber member in addition multiplied with the coefficient  $k_{mod}$ .

According to EN 1990 (Eurocode – Basis of design) paragraph 6.3.5 the design value of load-carrying capacity may be determined by reducing the characteristic values of the load-carrying capacity with different partial factors.

Thus, the characteristic values of the load–carrying capacity are determined also for combined timber and steel plate failure  $F_{Rk,T}$  (obtaining the compressive strength perpendicular to grain or the embedment strength of fasteners subjected to shear or the withdrawal capacity of the most loaded fastener, respectively) as well as for pure concrete or steel plate failure  $F_{Rk,C/S}$ . The design value of the load–carrying capacity is the smaller value of both load–carrying capacities.

$$F_{Rd} = min \left\{ \frac{k_{mod} \cdot F_{Rk,T}}{\gamma_{M,T}}; \frac{F_{Rk,C/S}}{\gamma_{M,C/S}} \right\}$$

Therefore, for combined timber and steel plate failure the load duration class and the service class are included. The different partial factors  $\gamma_M$  for concrete, steel or timber, respectively, are also correctly taken into account.

#### 3.5 Mechanical resistance and stability

See annex B for the characteristic load-carrying capacity in the different directions  $F_1$ ,  $F_2$ ,  $F_3$ ,  $F_4$  and  $F_5$ .

The characteristic capacities of the angle brackets and hold downs are determined by calculation assisted by testing and testing as described in the EAD 130186-00-0603. They should be used for designs in accordance with Eurocode 5 or a similar national Timber Code.

No performance has been assessed in relation to ductility of a joint under cyclic testing. The contribution to the performance of structures in seismic zones, therefore, has not been assessed.

Other connector nails or screws according to EN 14592 or ETA with the same or better performance than the fasteners given in table A.4 may be used.

# **3.6** Aspects related to the performance of the product 3.6.1 Corrosion protection in service class 1, 2 and 3. In accordance with EAD 130186-00-0603 the angle brackets and hold downs are produced from:

- steel S235 / Z 275 or FeZn12c treated according to EN 10025:2005 with  $R_e \ge 235$  N/mm²,  $R_m \le 510$  N/mm² and  $A_{80} \ge 26\%$
- steel S355 / Z 275 or FeZn12c treated according to EN 10025:2005 with  $R_e \ge$  355 N/mm²,
  - $R_{\rm m} \le 630 \text{ N/mm}^2 \text{ and } A_{80} \ge 22\%$
- steel S275 / Z 275 or FeZn12c according to EN 10025:2005 with  $R_e \geq$  275 N/mm²,  $R_m \leq$  560 N/mm² and  $A_{80} \geq$  23%
- steel DX51D / Z 275 or FeZn12c according to EN 10346:2015 with  $R_e \geq 235$  N/mm²,  $R_m \leq 500$  N/mm² and  $A_{80} \geq 22\%$
- steel S250GD / Z 275 according to EN 10346:2015 with  $R_e \ge 250$  N/mm²,  $R_m \le 470$  N/mm² and  $A_{80} \ge 19\%$
- steel S350GD / Z 275 according to EN 10346:2015 with  $R_e \ge 350$  N/mm²,  $R_m \ge 420$  N/mm² and  $A_{80} \ge 16\%$
- Stainless steel with  $R_e \geq 235 \ N/mm^2,$   $R_m \leq 630 \ N/mm^2$  and  $A_{80} \geq 22\%$

#### 3.7 General aspects related to the use of the product

The angle brackets and hold downs are manufactured in accordance with the provisions of this European Technical Assessment using the manufacturing processes as identified in the inspection of the plant by the notified inspection body and laid down in the technical documentation

The nailing pattern used shall be as defined in Annex A.

The following provisions apply:

- The structural members the components 1 and 2 shown in the figure on page 15 - to which the brackets are fixed shall be:
  - Restrained against rotation.
  - Strength class C14 or better, see section II.2 of this ETA
  - Free from wane under the bracket.
- The actual end bearing capacity of the timber member to be used in conjunction with the bracket is checked by the designer of the structure to ensure it is not less than the bracket capacity and, if necessary, the bracket capacity reduced accordingly.
- With the following exceptions, the minimum nail's or screw's end and edge distances according to EN 1995-1-1:2010 or ETA have to be provided for.
- End or edge distance in component 2 towards the angle brackets bend line (shown in the figure on page 17).
- Edge distance in component 2 timber members for member depth ≥ 38 mm: a<sub>4,t</sub> ≥ 13 mm

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a_{4,c} \ge 13 \text{ mm}
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• For CLT, minimum nail's end and edge distances

$$a_{3,t} = (7 + 3 \cos \alpha) d$$

 $a_{3,c} = 6 d$ 

$$a_{4,t} = (3 + 4 \cos \alpha) d$$

 $a_{4,c} = 3 d$ 

 $\alpha$  is the angle between load and grain direction of the outer layers.

 For CLT, minimum screw's spacing, end and edge distances are:

 $a_1 = 4 d$ 

 $a_2 = 2.5 d$ 

 $a_{3,t} = 6 d$ 

 $a_{3,c} = 6 d$ 

 $a_{4,t} = 6 d$ 

 $a_{4,c} = 2.5 d$ 

 $\alpha$  is the angle between load and grain direction of the outer layers.

- The soundproofing interlayer of NINO angle brackets shall be arranged between the horizontal flange and the timber member (component 1 as shown in the figure on page 19).
- There are no specific requirements relating to preparation of the timber members.

The execution of the connection shall be in accordance with the assessment holder's technical literature.

4 Assessment and verification of constancy of performance (hereinafter AVCP) system applied, with reference to its legal base

#### 4.1 AVCP system

According to the decision 97/638/EC of the European Commission1, as amended, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is 2+.

# 5 Technical details necessary for the implementation of the AVCP system, as provided for in the applicable EAD

Technical details necessary for the implementation of the AVCP system are laid down in the control plan deposited at ETA-Danmark prior to CE marking.

Issued in Copenhagen on 2024-12-13 by

Thomas Bruun

Managing Director, ETA-Danmark

## Annex A Product details definitions

Table A.1 Materials specification

Angle Bracket type	Thickness	Steel specification	Coating				
	(mm)		specification				
NINO100100	2,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
NINO15080	2,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
NINO15080S	2,5	S355/S350GD	FeZn12c / Z 275				
NINO100200	3,0	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
WKR9530	3,0	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
WKR13535	3,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
WKR21535	3,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
WKR28535	3,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
WKR41035	3,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
WKR53035	3,5	S235/S355/S275/DX51D/S250GD	FeZn12c / Z 275				
Washer NINOW15080	6,0	S235/S355/S275	-				
Washer NINOW100200	8,0	S235/S355/S275	-				
Note: Steel with equivalent or	Note: Steel with equivalent or superior mechanical properties may also be used						

Table A.2 Materials specification – Soundproofing Interlayer for NINO angle brackets

Soundproofing interlayer type	Thickness (mm)
Xylofon or Xylofonplate	6,0

Table A.3 Range of sizes

Angle Bracket type	_	t (mm)			Widtl	n (mm)
NINO100100	99	101	77	79	103	105
NINO15080	76	78	54	56	145	147
NINO15080S	93	95	54	56	155	157
NINO100200	196	198	121	123	103	105
WKR9530	94	96	84	86	64	66
WKR13535	134	136	84	86	64	66
WKR21535	214	216	84	86	64	66
WKR28535	284	286	84	86	64	66
WKR41035	409	411	84	86	64	66
WKR53035	529	531	84	86	64	66
Washer NINOW15080	-	-	49	51	145	147
Washer NINOW100200	-	-	119	121	103	105

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Table A.4 Fastener specification

Fastener	Minimum Length	Minimum Threaded Length	Fastener type
Rotho Blaas nail 4.0 mm, type LBA	40 mm	30 mm	Ringed shank nails according to ETA-22/0002
Ringed shank nail 4.0 mm	40 mm	30 mm	Ringed shank nails according to EN 14592
Rotho Blaas screw 5.0 mm, type LBS	40 mm	35 mm	Self-tapping screws according to ETA-11/0030
Rotho Blaas screw 8.0 mm, type HBSPL	100 mm	75 mm	Self-tapping screws according to ETA-11/0030
Rotho Blaas screw 10.0 mm, type HBS or HBSP or TBS	60 mm	48 mm	Self-tapping screws according to ETA-11/0030
Rotho Blaas screw 12.0 mm, type HBS or HBSP	80 mm	48 mm	Self-tapping screws according to ETA-11/0030
Rotho Blaas screw 9.0 mm, type VGS	100 mm	90 mm	Self-tapping screws according to ETA-11/0030
Rotho Blaas screw 11.0 mm, type VGS	60 mm	50 mm	Self-tapping screws according to ETA-11/0030
Rotho Blaas screw 13.0 mm, type VGS	75 mm	60 mm	Self-tapping screws according to ETA-11/0030

In the load-carrying-capacities of the nailed or with 5.0 mm screwed connection in Annex B the capacities calculated from the formulas of Eurocode 5 are used assuming a thick steel plate when calculating the lateral fastener load-carrying-capacity. For the connection with screws with larger diameter than 5.0 mm a thin steel plate is assumed. The load-carrying-capacities of the angle brackets and hold downs have been determined based on the use of Rotho Blaas nail 4.0 mm, type LBA in accordance with ETA-22/0002 and self-tapping screws according to ETA-11/0030. The characteristic withdrawal capacity of the nails or screws has to be determined by calculation in accordance with EN 1995-1-1:2010, paragraph 8.3.2:

$$F_{ax,Rk} = f_{ax,k} \cdot d \cdot t_{pen} \left(\frac{\rho_k}{350}\right)^{0.8}$$
 for the nails 4.0 mm

$$F_{ax,\alpha,Rk} = min \left\{ f_{tens,k}; \frac{n_{ef} \cdot k_{ax} \cdot f_{ax,k} \cdot d \cdot \ell_{ef}}{k_{\beta}} \left( \frac{\rho_{k}}{\rho_{a}} \right)^{0,8} \right\} \quad \text{ for the screws}$$

where:

n<sub>ef</sub> Effective number of fasteners

 $f_{ax,k}$  Characteristic value of the withdrawal parameter in N/mm<sup>2</sup>

d Nail or screw diameter in mm

t<sub>pen</sub> Penetration depth of the ringed shank including the nail tip in mm

 $\rho_k$  Characteristic density of the timber in kg/m<sup>3</sup>

 $\rho_a$  Characteristic density of the timber in kg/m<sup>3</sup> according to  $f_{ax,k}$ 

 $f_{ax,k}$ ,  $f_{tens,k}$ ,  $\rho_a$ ,  $k_{ax}$  and  $k_{\beta}$  see ETA-11/0030 or ETA-22/0002.

The shape of the nail or LBS or HBSP screw directly under the head shall be in the form of a truncated cone with a diameter under the head which fits the hole diameter. TBS screws shall have a large washer head.

Head pull-through is relevant for HBS, HBSP, VGS screws without washer.

<b>Bolts diameter</b>	Correspondent hole diameter	<b>Bolts type</b>
12.0 mm	Max. 2 mm larger than the bolt diameter	See specification of the manufacturer

Metal Anchors diameter	Correspondent Hole diameter	Anchors type
12.0 mm	Max. 2 mm larger than the anchor diameter	See specification of the manufacturer

## Annex B Characteristic load-carrying capacities and slip moduli

Table B.1: Force F<sub>1</sub>, 1 angle bracket / connection timber to timber

		Timber-to-ti	350 kg/m <sup>3</sup>	
NINO Angle bracket	Fastener pattern	$\mathbf{F}_{1,\mathrm{Rk}}$	F <sub>1,Rk</sub> [kN]	
		LBA nails 4x60 <sup>c</sup>	LBA nails 4x60 ° LBS screws 5x50 d	
NINO100100 a	1	20,0	20,0	$F_{1,Rk}/6$
NINO100100	2	5,9	6,8	$F_{1,Rk}/2$
NINO15080 a	1	37,2/39,5 b	37,2/39,5 b	$F_{1,Rk}/6$
NINO15080	2	4,0	6,0	$F_{1,Rk}/2$
NINO15080	3	4,0	6,0	$F_{1,Rk}/2$
NINO15080	4	4,0	6,0	$F_{1,Rk}/2$
NINO15080	5	4,0	6,0	$F_{1,Rk}/2$
NINO100200 a	1	41,2	41,2	$F_{1,Rk}/5$

<sup>&</sup>lt;sup>a</sup> Load-carrying capacity is based on VGS screws  $\varnothing$  9xL and L  $\ge$  140 mm. For L < 140 mm,  $F_{1,Rk}$  is reduced with the ratio L/140.

**Table B.2:** Force F<sub>1</sub>, 1 angle bracket / connection timber to timber

NINO Anglo	Fastanan	Timber-to-timber connection $\rho_k = 350 \text{ kg/m}^3$					
NINO Angle bracket	Fastener pattern	$F_{1,Rk}$ [kN]	V. [kN/mm]				
bracket	pattern	HBSPL screws $8x100$ or $8xL$ where $L > 100$ mm	$K_{1,ser}$ [kN/mm]				
NINO15080S	1	49,9	F <sub>1,Rk</sub> /5				
NINO15080S	2	32,0	F <sub>1,Rk</sub> /5				
Note: Values ap	Note: Values apply to installation with or without 6 mm Xylofon						

**Table B.3:** Force F<sub>1</sub>, 1 angle bracket / connection timber to rigid support

NINO Anglo	Fastanan	Timber-to-concrete connection without washe	$er \rho_k = 350 \text{ kg/m}^3$					
NINO Angle bracket	pattern	Fastener  Pattern  F <sub>1,Rk</sub> [kN]		K <sub>1,ser</sub> [kN/mm]				
Diacket	pattern	HBSPL screws 8x100 or 8xL where L > 100 mm	$\mathbf{k}_{t/\!/}$	K1,ser [KIN/IIIII]				
NINO15080S	3	22,9	1,36	$F_{1,Rk}/5$				
NINO15080S	4	18,4	1,36	$F_{1,Rk}/5$				
Note: Values ap	Note: Values apply to installation with timber, glulam or CLT							

<sup>&</sup>lt;sup>b</sup> The first value relates to connection with soundproofing interlayer, the second without.

<sup>&</sup>lt;sup>c</sup> For LBA nails with shorter length,  $F_{1,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{1,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

For LBS screws with shorter length,  $F_{1,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ Note: the most severe applicable reduction of a, c or d applies.

**Table B.4:** Force F<sub>1</sub>, 1 angle bracket / Load-carrying capacity of fasteners in the vertical flange and of the steel - connection timber to rigid support

			Timber-to-rigid support connection $\rho_k = 350 \text{ kg/m}^3$							
NINO	Fas-		F <sub>1,Rk</sub> [kN]				F <sub>1,Rk</sub> [kN]			
Angle	tener		withou	ut washer			with N	W washe	r	
bracket	pattern	LBA	LBS	Bolts	$\mathbf{K}_{1,\mathrm{ser}}$	LBA	LBS	Bolts	$\mathbf{K}_{1,\mathrm{ser}}$	
brucket	pattern	nails	screws	inner	[kN/mm]	nails	screws	inner	[kN/mm]	
		4x60 a	5x50 b	row k <sub>t//</sub>		4x60 a	5x50 b	$row k_{t//}$	[KIN/IIIII]	
NINO100100	6	14,0	14,0	1,21	$F_{1,Rk}/18$	-	-	-	-	
NINO100100	7	14,0	14,0	1,21	$F_{1,Rk}/18$	-	-	-	-	
NINO15080	6	14,7	14,7	1,38	$F_{1,Rk}/16$	24,9	20,9	1,75	$F_{1,Rk}/8$	
NINO15080	7	14,7	14,7	1,38	$F_{1,Rk}/16$	24,9	24,9	1,75	$F_{1,Rk}/8$	
NINO15080	8	14,7	14,7	1,38	$F_{1,Rk}/16$	24,9	22,5	1,75	$F_{1,Rk}/8$	
NINO15080	9	14,7	14,7	1,38	$F_{1,Rk}/16$	24,9	22,5	1,75	$F_{1,Rk}/8$	
NINO15080	10	13,3	11,3	1,38	$F_{1,Rk}/16$	13,3	11,3	1,75	$F_{1,Rk}/8$	
NINO15080	11	13,3	11,3	1,38	$F_{1,Rk}/16$	13,3	11,3	1,75	$F_{1,Rk}/8$	
NINO100200	2T/2P	14,7	14,7	1,11	$F_{1,Rk}/16$	34,7	29,3	1,23	$F_{1,Rk}/8$	
NINO100200	3T/3P	14,7	14,7	1,11	$F_{1,Rk}/16$	34,7	34,7	1,23	$F_{1,Rk}/8$	
NINO100200	4T/4P	14,7	14,7	1,11	$F_{1,Rk}/16$	34,7	34,7	1,23	$F_{1,Rk}/8$	
NINO100200	5T/5P	14,7	14,7	1,11	$F_{1,Rk}/16$	34,7	34,7	1,23	$F_{1,Rk}/8$	
NINO100200	6T/6P	14,7	14,7	1,11	F <sub>1,Rk</sub> /16	34,7	34,7	1,23	F <sub>1,Rk</sub> /8	
NINO100200	7T/7P	14,7	14,7	1,11	F <sub>1,Rk</sub> /16	34,7	34,7	1,23	F <sub>1,Rk</sub> /8	

For LBA nails with shorter length,  $F_{1,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{1,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

**Table B.5:** Force  $F_{2/3}$ , 1 angle bracket / connection timber to timber

NINO Amala	Eastonon	Timber-to-timber connection $\rho_k = 350 \text{ kg/m}^3$					
NINO Angle bracket	Fastener pattern  F <sub>2/3,Rk</sub> [kN]  K <sub>2/3 ser</sub> [kN]		I/ [lrN/mm]				
DIACKCE	pattern	HBSPL screws 8x100 or 8xL where L > 100 mm	$\mathbf{K}_{2/3,\mathrm{ser}}\left[\mathbf{kN/mm}\right]$				
NINO15080S	1	35,0	$F_{2/3,Rk}/5$				
NINO15080S	2	25,8	$F_{2/3,Rk}/5$				
Note: Values app	Note: Values apply to installation with or without 6 mm Xylofon						

**Table B.6:** Force  $F_{2/3}$ , 1 angle bracket / connection timber to rigid support

NINO Anglo	Fostonov	Timber-to-concrete connection without was	sher $\rho_k = 350 \text{ kg/m}^3$	
NINO Angle bracket	Fastener pattern	F <sub>2/3,Rk</sub> [kN]	K <sub>2/3,ser</sub> [kN/mm]	
Dracket	pattern	HBSPL screws 8x100 or 8xL where L > 100 mm	<b>M</b> 2/3,ser [KIN/IIIII]	
NINO15080S	3	41,3	$F_{2/3,Rk}/5$	
NINO15080S	4	22,6	$F_{2/3,Rk}/5$	

Shear loads per bolt or metal anchor, see Figure below ( $e_z = 0$ ):

- In x-direction:  $\pm 0.5 \cdot F_{2/3,Ed}$ ,
- In y-direction:  $\pm 0.29 \cdot F_{2/3,Ed}$ .

Note: Values apply to installation with timber, glulam or CLT

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length,  $F_{1,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

**Table B.7:** Force  $F_{2/3}$ , 1 angle bracket / connection timber to timber

NINO		F	$F_{2/3,Rk}$ [kN] for timber-to-timber connection $\rho_k=350~kg/m^3$					
NINO Angle	Fastener	LB	A nails 4x60 <sup>a</sup>	LB	S screws 5x50 b	W.		
bracket	pattern	No inter-	6 mm soundproofing	No inter-	6 mm soundproofing	K <sub>2/3,ser</sub> [kN/mm]		
Бтисисс		layer	interlayer	layer	interlayer			
NINO100100 <sup>c</sup>	1	38,1	34,6	18,5	16,9	$F_{2/3,Rk}/5$		
NINO100100	2	17,2	9,4	9,5	7,4	$F_{2/3,Rk}/5$		
NINO100100	3	9,8	8,9	9,1	7,4	$F_{2/3,Rk}/5$		
NINO100100	4	11,3	9,4	9,5	7,4	$F_{2/3,Rk}/5$		
NINO100100	5	9,8	8,9	9,0	7,4	$F_{2/3,Rk}/5$		
NINO15080 <sup>c</sup>	1	38,1	34,6	27,6	25,5	$F_{2/3,Rk}/5$		
NINO15080	2	15,5	13,0	13,1	10,2	$F_{2/3,Rk}/5$		
NINO15080	3	13,3	12,3	12,3	10,1	$F_{2/3,Rk}/5$		
NINO15080	4	15,5	13,0	13,1	10,2	$F_{2/3,Rk}/5$		
NINO15080	5	12,7	11,8	11,2	10,0	$F_{2/3,Rk}/5$		
NINO100200°	1	26,7	18,7	18,7	17,2	F <sub>2/3,Rk</sub> /6		

<sup>&</sup>lt;sup>a</sup> For LBA nails with shorter length,  $F_{2/3,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{2/3,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

Note: the most severe applicable reduction of a, b or c applies.

Table B.8: Force F<sub>2/3</sub>, 1 angle bracket / connection timber to rigid support with or without NINOW washer

NINO Angle	Fastener	F <sub>2/3,Rk</sub> [kN] for timber-t	o- rigid sup	port connection $\rho_k =$	350 kg/m <sup>3</sup>
bracket	pattern	LBA nails 4x60 a		LBS screws 5x50 b	
NINO100100	6	18,1	78,5	7,2	$F_{2/3,Rk}/5$
NINO100100	7	18,1	54,5	9,8	$F_{2/3,Rk}/5$
NINO100100	8	5,8	0	4,9	$F_{2/3,Rk}/5$
NINO100100	9	7,8	0	6,6	$F_{2/3,Rk}/5$
NINO100100	10	11,2	0	9,4	$F_{2/3,Rk}/5$
NINO100100	11	9,3	42,5	4,2	$F_{2/3,Rk}/2$
NINO100100	12	9,3	22,5	6,3	$F_{2/3,Rk}/2$
NINO15080	6	26,7 with / 21,1 without washer	66,5	7,9	$F_{2/3,Rk}/4$
NINO15080	7	21,3	0	17,9	$F_{2/3,Rk}/4$
NINO15080	8	11,0	0	9,3	$F_{2/3,Rk}/4$
NINO15080	9	15,7	0	13,2	$F_{2/3,Rk}/4$
NINO15080	10	9,3	0	6,0	$F_{2/3,Rk}/4$
NINO15080	11	10,0	0	8,5	$F_{2/3,Rk}/4$
NINO100200	2T/2P	11,6 with / 8,3 without washer	174,5	3,5	$F_{2/3,Rk}/3$
NINO100200	3T/3P	10,7	162,5	6,0	$F_{2/3,Rk}/3$
NINO100200	4T/4P	10,7	138,5	7,0	$F_{2/3,Rk}/3$
NINO100200	5T/5P	16,9	114,5	8,3	$F_{2/3,Rk}/3$
NINO100200	6T/6P	16,9	90,5	10,1	$F_{2/3,Rk}/3$
NINO100200	7T/7P	16,9	66,5	13,2	$F_{2/3,Rk}/3$

Shear loads per bolt or metal anchor, see Figure below:

- In x-direction:  $\pm$  0,5 · F<sub>2/3,Ed</sub> for NINO100100, NINO15080 and the inner bolt row of NINO100200,  $\pm$  0,01 · F<sub>2/3,Ed</sub> for the outer bolt row of NINO100200
- In y-direction:  $\pm 0,43 \cdot F_{2/3,Ed}$  for NINO100100 or NINO100200 with two bolts close to the bend line,  $\pm 0,25 \cdot F_{2/3,Ed}$  for NINO15080 and the inner bolt row of NINO100200 with four bolts.

 $<sup>^</sup>b \ For \ LBS \ screws \ with \ shorter \ length, \ F_{2/3,Rk} \ must \ be \ reduced \ by \ min\{F_{v,short,Rk}/F_{v,50,Rk}\ ; \ F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

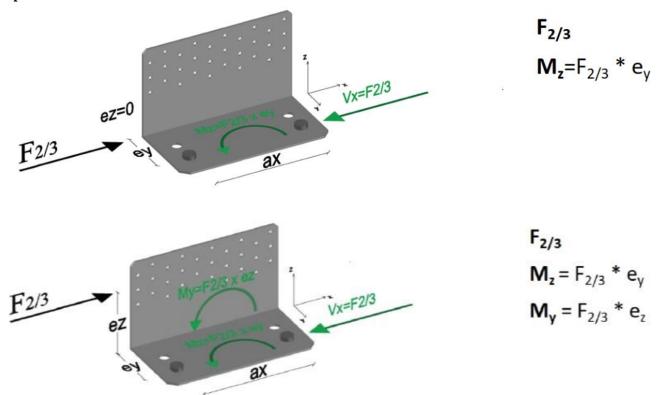
<sup>&</sup>lt;sup>c</sup> Load-carrying capacity is based on VGS screws  $\varnothing$  9xL and L  $\geq$  140 mm. For L  $\leq$  140 mm,  $F_{2/3,Rk}$  is reduced with the ratio L/140.

<sup>&</sup>lt;sup>a</sup> For LBA nails with shorter length,  $F_{2/3,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{2/3,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length, F<sub>2/3,Rk</sub> must be reduced by min{F<sub>v,short,Rk</sub>/F<sub>v,50,Rk</sub>; F<sub>ax,short,Rk</sub>/F<sub>ax,50,Rk</sub>}

<sup>&</sup>lt;sup>c</sup> For nailed connections, for screwed connections  $e_z = 0$ 

#### Explanation for footnotes in Table B.6 and B.8



**Table B.9:** 1 angle bracket for force  $F_4$  and  $F_5$ , and 2 angle brackets for force  $F_{4/5}$  / connection timber to timber with or without soundproofing interlayer

NINO	F 4		Timber-to-timber connection $\rho_k = 350 \text{ kg/m}^3$						
Angle	Fastener pattern	LI	LBA nails 4x60 <sup>a</sup>		LB	S screws 5x5	50 b	K <sub>4,ser</sub>	
bracket	pattern	F <sub>4,Rk</sub> [kN]	F <sub>5,Rk</sub> [kN]	F <sub>4/5,Rk</sub> [kN]	F <sub>4,Rk</sub> [kN]	F <sub>5,Rk</sub> [kN]	F <sub>4/5,Rk</sub> [kN]	[kN/mm]	
NINO100100°	1	23,2	1,8	25,0	22,0	1,8	23,8	$F_{4,Rk}/1,5$	
NINO100100	2	23,2	1,8	25,0	22,0	1,8	23,8	$F_{4,Rk}/1,5$	
NINO100100	3	7,4	1,8	9,2	7,4	1,8	9,2	$F_{4,Rk}/1,5$	
NINO100100	4	23,2	3,4	26,6	22,0	3,4	25,4	$F_{4,Rk}/1,5$	
NINO100100	5	9,2	3,4	12,6	9,2	3,4	12,6	$F_{4,Rk}/6$	
NINO15080°	1	22,3	2,5	24,8	21,6	2,5	24,1	$F_{4,Rk}/1,5$	
NINO15080	2	22,3	2,5	24,8	21,6	2,5	24,1	$F_{4,Rk}/1,5$	
NINO15080	3	10,2	2,5	12,7	10,2	2,5	12,7	$F_{4,Rk}/1,5$	
NINO15080	4	18,7	4,8	23,5	17,7	4,8	22,5	$F_{4,Rk}/1,5$	
NINO15080	5	14,7	4,8	19,5	14,7	4,8	19,5	F <sub>4,Rk</sub> /6	
NINO100200°	1	19,1	2,6	21,7	19,1	2,6	21,7	$F_{4,Rk}/1,5$	

 $<sup>\</sup>overline{\ }^a$  For LBA nails with shorter length,  $F_{4,Rk}$  or  $F_{5,Rk}$  must be reduced by  $\min\{F_{v,short,Rk}/F_{v,60,Rk}\ ;\ F_{ax,short,Rk}/F_{ax,60,Rk}\ For\ ringed\ shank\ nails\ according\ to\ EN\ 14592,\ F_{4,Rk}\ or\ F_{5,Rk}\ must\ be\ reduced\ by\ min\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}\ ;\ F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

**Table B.10:** 1 angle bracket for force F<sub>4</sub> and F<sub>5</sub>, and 2 angle brackets for force F<sub>45</sub> / connection timber to timber

		Timber-to-timber connection $\rho_k = 350 \text{ kg/m}^3$					
NINO Angle bracket	Fastener pattern	tern HBSPL screws 8x100 or 8xL where L > 100 mm					
		F <sub>4,Rk</sub> [kN]	F <sub>5,Rk</sub> [kN]	F <sub>45,Rk</sub> [kN]			
NINO15080S	1	18,9	2,4	21,3			
NINO15080S	2	14,2	2,4	16,6			
Note: Values apply to installation with or without 6 mm Xylofon							

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length,  $F_{4,Rk}$  or  $F_{5,Rk}$  must be reduced by min{ $F_{v,short,Rk}$ / $F_{v,50,Rk}$ ;  $F_{ax,short,Rk}$ / $F_{ax,50,Rk}$ } <sup>c</sup> Load-carrying capacity is based on VGS screws Ø 9xL and L ≥ 100 mm.

**Table B.11:** 1 angle bracket for force  $F_4$  and  $F_5$ , and 2 angle brackets for force  $F_{4/5}$  / connection timber to rigid support

NINO	<b>T</b>	Ti	mber-to-rig	id support co	nnection ρ <sub>k</sub>	=350  kg/m	3	
Angle	Fastener pattern	LB	A nails 4x60	a	LF	LBS screws 5x50 b		
bracket	pattern	F <sub>4,Rk</sub> [kN]	F <sub>5,Rk</sub> [kN]	F <sub>4/5,Rk</sub> [kN]	F <sub>4,Rk</sub> [kN]	F <sub>5,Rk</sub> [kN]	F <sub>4/5,Rk</sub> [kN]	
NINO100100	6	6,2	1,1	7,4	6,2	1,1	7,4	
NINO100100	7	23,2	1,8	25,0	22,0	1,8	23,8	
NINO100100	8	3,8	1,1	5,0	3,8	1,1	5,0	
NINO100100	9	7,4	1,8	9,2	7,4	1,8	9,2	
NINO100100	10	14,4	3,4	17,8	13,6	3,4	17,0	
NINO100100	11	6,3	1,8	8,1	5,9	1,8	7,7	
NINO100100	12	9,2	3,4	12,6	9,2	3,4	12,6	
NINO15080	6	8,7	1,6	10,3	8,7	1,6	10,3	
NINO15080	7	22,3	2,5	24,8	21,6	2,5	24,1	
NINO15080	8	10,2	2,5	12,7	10,2	2,5	12,7	
NINO15080	9	18,7	4,8	23,5	17,7	4,8	22,5	
NINO15080	10	8,4	2,5	10,9	7,9	2,5	10,4	
NINO15080	11	11,6	4,8	16,4	11,6	4,8	16,4	
NINO100200	2T/2P	2,1	0,7	2,8	2,1	0,7	2,8	
NINO100200	3T/3P	2,6	0,8	3,4	2,6	0,8	3,4	
NINO100200	4T/4P	3,4	1,0	4,4	3,4	1,0	4,4	
NINO100200	5T/5P	4,9	1,2	6,1	4,9	1,2	6,1	
NINO100200	6T/6P	8,5	1,7	10,2	8,5	1,7	10,2	
NINO100200	7T/7P	19,1	2,6	21,7	19,1	2,6	21,7	

For LBA nails with shorter length,  $F_{4,Rk}$  or  $F_{5,Rk}$  or  $F_{45,Rk}$  must be reduced by

 $min\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$ 

For ringed shank nails according to EN 14592,  $F_{4,Rk}$  or  $F_{5,Rk}$  or  $F_{45,Rk}$  must be reduced by

 $min\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}\ ;\ F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

 $min\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

**Table B.12:** 1 angle bracket for force  $F_4$  and  $F_5$ , and 2 angle brackets for force  $F_{4/5}$  / connection timber to rigid support

		Timber-to-concrete connection without washer $\rho_k = 350 \text{ kg/m}^3$				
NINO Angle bracket	Fastener pattern	HBSPL screv	vs 8x100 or 8xL where	e L > 100 mm		
		F <sub>4,Rk</sub> [kN]	F <sub>5,Rk</sub> [kN]	F <sub>45,Rk</sub> [kN]		
NINO15080S	3 CLT	18,9	2,3	21,3		
NINO15080S	4 CLT	14,2	1,4	15,6		
NINO15080S	3 glulam	17,6	2,4	20,0		
NINO15080S	4 glulam	13,6	1,4	15,0		

For LBS screws with shorter length,  $F_{4,Rk}$  or  $F_{5,Rk}$  or  $F_{45,Rk}$  must be reduced by

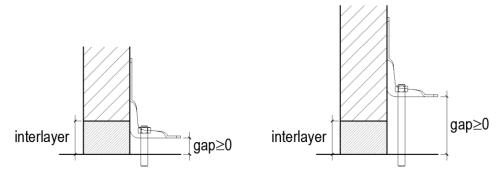
**Table B.13:** Force F<sub>1</sub>, 1 hold-down / connection timber to timber or timber to rigid support

WIZD	T 4	Conne	Connections without gap $\rho_k = 350 \text{ kg/m}^{3 \text{ c}}$						
WKR hold down	Fastener pattern	F <sub>1,no ga</sub>	<sub>p,Rk</sub> [kN]	1-	K <sub>1,ser</sub>				
noid down	pattern	LBA nails 4x60 a	LBS screws 5x50 b	$\mathbf{k}_{t}$	[kN/mm]				
WKR9530	1-2	Min{15,0 $^{1}$ ; $F_{ax,Rk}/k_t$ }	Min{13,3 <sup>1</sup> ; $F_{ax,Rk}/k_t$ }	1,05	F <sub>1,Rk</sub> /4				
WKR13535	1-2	Min{28,31; $F_{ax,Rk}/k_t$ }	$Min\{24,6^{1}; F_{ax,Rk}/k_t\}$	1,05	$F_{1,Rk}/4$				
WKR21535	4	Min{8,0 <sup>1</sup> ); $F_{ax,Rk}/k_t$ }	$Min\{6,8^{1}; F_{ax,Rk}/k_t\}$	1,45	$F_{1,Rk}/4$				
WKR21535	3	Min{18,7 $^{1}$ ; $F_{ax,Rk}/k_t$ }	Min{15,8 <sup>1</sup> ; $F_{ax,Rk}/k_t$ }	1,45	$F_{1,Rk}/4$				
WKR21535	1-2	Min{ $47,0^{1}$ ; $F_{ax,Rk}/k_t$ }	$Min\{40,3^{1}; F_{ax,Rk}/k_t\}$	1,10	$F_{1,Rk}/4$				
WKR28535	5	Min{21,3 $^{1}$ ; $F_{ax,Rk}/k_t$ }	Min{18,0 $^{1}$ ; $F_{ax,Rk}/k_t$ }	1,45	$F_{1,Rk}/4$				
WKR28535	1-4	Min{37,31; $F_{ax,Rk}/k_t$ }	Min{36,0 $^{1}$ ; $F_{ax,Rk}/k_t$ }	1,45	$F_{1,Rk}/4$				
WKR28535	2-3	Min{57,6 <sup>1</sup> ; $F_{ax,Rk}/k_t$ }	$Min{49,3^1}; F_{ax,Rk}/k_t}$	1,10	$F_{1,Rk}/4$				
WKR41035	2	Min{37,31; $F_{ax,Rk}/k_t$ }	$Min{31,5^1}; F_{ax,Rk}/k_t$	1,45	$F_{1,Rk}/4$				
WKR41035	1	$Min{45,3^1}; F_{ax,Rk}/k_t}$	Min{38,31; $F_{ax,Rk}/k_t$ }	1,45	F <sub>1,Rk</sub> /4				
WKR53035	1-2	Min{42,6 <sup>1</sup> ); $F_{ax,Rk}/k_t$ }	Min{36,0 <sup>1</sup> ; $F_{ax,Rk}/k_t$ }	1,45	$F_{1,Rk}/4$				

<sup>&</sup>lt;sup>1)</sup> For nails in CLT,  $a_{3,t}$  may be reduced to 40 mm, for screws in CLT to 30 mm. For nails in CLT and  $a_{3,t}$  < 60 mm, the value must be decreased by 7 %.

 $F_{ax,Rk}$  is the axial load-carrying capacity of a metal anchor in concrete or a bolt in a timber or steel member or a screw according to ETA-11/0030 in a timber member. The head pull-through capacity of a fastener in the horizontal flap may be assumed according to Table B.8.

#### Explanation for connections with gap in Table B.7



**Table B.14:** Force F<sub>1</sub>, head pull-through capacity of a fastener in the horizontal flange

Fastener			Fhead, Rk [kN]		
rastener	WKR9530	WKR13535	WKR21535	WKR28535	WKR53035
Metal anchor M12 or bolt M12 in hold-down without gap	26	26	26	26	26
Metal anchor M12 or bolt M12 in hold-down with gap	8,3	19	19	19	19
Rotho Blaas screw type HBS or TBS Ø10 mm or Ø12 mm or VGS Ø11 mm or Ø13 mm with washer HUS or with large washer head according to ETA-11/0030	f <sub>tens,k</sub>				
Rotho Blaas screw type HBSP Ø10 mm with WU2 washer head according to ETA-11/0030	20	21	21	21	21
Rotho Blaas screw type HBSP Ø12 mm with WU2 washer head according to ETA-11/0030	27	29	29	29	29

<sup>&</sup>lt;sup>a</sup> For LBA nails with shorter length,  $F_{1,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{1,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length,  $F_{1,Rk}$  must be reduced by  $min\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

<sup>&</sup>lt;sup>c</sup> For connections with gap,  $k_t = 1.0$  and  $F_{1,gap,Rk} = Min\{F_{1,no\ gap,Rk}; 19\ kN\}$ 

**Table B.15:** Force F<sub>4</sub>, 1 hold-down / connection timber to timber

		F <sub>4,Rk</sub> [kN] for timber-to-timber connection						
WKR hold	Fastener	r	no interlayer		interl	interlayer up to 20 mm		
down	pattern	LBA nails 4x60 <sup>a</sup>	LBS screws 5x50 b	K <sub>4,ser</sub> [kN/mm]	LBA nails 4x60 <sup>a</sup>	LBS screws 5x50 b	K <sub>4,ser</sub> [kN/mm]	
WKR9530	2	Min{14,7; F <sub>vh,Rk</sub> }	Min{14,1; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{11,3; Fvh,Rk}	Min{10,7; F <sub>vh,Rk</sub> }	F4,Rk/6	
WKR13535	2	Min{18,3; F <sub>vh,Rk</sub> }	Min{17,2; F <sub>vh,Rk</sub> }	F <sub>4,Rk</sub> /6	Min{14,9; Fvh,Rk}	Min{13,8; F <sub>vh,Rk</sub> }	F4,Rk/6	
WKR21535	2	Min{23,0; Fvh,Rk}	Min{21,1; Fvh,Rk}	F <sub>4,Rk</sub> /6	Min{19,6; Fvh,Rk}	Min{17,7; F <sub>vh,Rk</sub> }	F4,Rk/6	
WKR28535	3	Min{25,6; F <sub>vh,Rk</sub> }	Min{23,4; Fvh,Rk}	F <sub>4,Rk</sub> /6	Min{22,3; Fvh,Rk}	Min{20,0; F <sub>vh,Rk</sub> }	F4,Rk/6	

<sup>&</sup>lt;sup>a</sup> For LBA nails with shorter length,  $F_{4,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{4,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

 $F_{vh,Rk}$  is the lateral load-carrying capacity of a metal anchor in concrete or a bolt in a timber or steel member or a screw according to ETA-11/0030 in a timber member.

Table B.16: Force F<sub>4</sub>, 1 hold-down / connection timber to rigid support

			F <sub>4,Rk</sub> [kN] 1	for timber-	to-rigid sup	port connectio	n		
WKD	Eastonon	n	no interlayer			interlayer thickness up to d <sub>ILmax</sub>			
WKR hold down	Fastener pattern	LBA nails 4x60 <sup>a</sup>	LBS screws 5x50 b	K <sub>4,ser</sub> [kN/mm]	LBA nails 4x60 <sup>a</sup>	LBS screws 5x50 b	d <sub>ILmax</sub> [mm]	K <sub>4,ser</sub> [kN/mm]	
WKR9530	1	Min{14,7; Fvh,Rk}	Min{14,1; Fvh,Rk}	F4,Rk/6	Min{11,3; Fvh,Rk}	Min{10,7; F <sub>vh,Rk</sub> }	20	F <sub>4,Rk</sub> /6	
WKR13535	1	Min{18,3; F <sub>vh,Rk</sub> }	Min{17,2; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{14,9; Fvh,Rk}	Min{13,8; F <sub>vh,Rk</sub> }	20	F4,Rk/6	
WKR21535	1	Min{23,0; F <sub>vh,Rk</sub> }	Min{21,1; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{19,6; F <sub>vh,Rk</sub> }	$\begin{array}{c} Min\{17,7;\\ F_{vh,Rk}\} \end{array}$	20	F4,Rk/6	
WKR28535	1-4	Min{21,7; F <sub>vh,Rk</sub> }	Min{20,0; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{13,0; Fvh,Rk}	Min{11,3; F <sub>vh,Rk</sub> }	120	F4,Rk/6	
W KK26333	2	Min{25,6; F <sub>vh,Rk</sub> }	Min{23,4; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{22,3; Fvh,Rk}	Min{20,0; F <sub>vh,Rk</sub> }	20	F <sub>4,Rk</sub> /6	
WKR41035	1	Min{22,3; Fvh,Rk}	Min{20,6; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{12,5; Fvh,Rk}	Min{10,8; F <sub>vh,Rk</sub> }	240	F4,Rk/6	
WKR53035	1-2	Min{21,7; F <sub>vh,Rk</sub> }	Min{20,0; F <sub>vh,Rk</sub> }	F4,Rk/6	Min{11,5; Fvh,Rk}	Min{9,8; F <sub>vh,Rk</sub> }	360	F4,Rk/6	

 $<sup>^</sup>a$  For LBA nails with shorter length,  $F_{4,Rk}$  must be reduced by  $min\{F_{v,short,Rk}/F_{v,60,Rk}\,;\,F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{4,Rk}$  must be reduced by  $min\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}\,;\,F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

 $F_{vh,Rk}$  is the lateral load-carrying capacity of a metal anchor in concrete or a bolt in a timber or steel member or a screw according to ETA-11/0030 in a timber member.

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length,  $F_{4,Rk}$  must be reduced by  $min\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

 $<sup>^</sup>b \ For \ LBS \ screws \ with \ shorter \ \underline{length}, \ F_{4,Rk} \ must \ be \ reduced \ by \ min \{F_{v,short,Rk}/F_{v,50,Rk} \ ; \ F_{ax,short,Rk}/F_{ax,50,Rk} \}$ 

**Table B.17:** Force F<sub>5</sub>, 1 hold-down / connection timber to timber

WZD I II	T 4	Timber	-to-timber connection	
WKR hold down	Fastener pattern	$\mathbf{F}_{5,R}$	k [kN]	( []
down	pattern	LBA nails 4x60 a	LBS screws 5x50 b	$\ell_{\rm BL}$ [mm]
WKR9530	2	2,6	3,4	70
WKR13535	2	2,6	3,6	70
WKR21535	2	2,6	3,6	70
WKR28535	3	2,6	3,6	70

<sup>&</sup>lt;sup>a</sup> For LBA nails with shorter length,  $F_{5,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,60,Rk}; F_{ax,short,Rk}/F_{ax,60,Rk}\}$  For ringed shank nails according to EN 14592,  $F_{5,Rk}$  must be reduced by min $\{F_{v,EN14592,Rk}/F_{v,LBA,Rk}; F_{ax,EN14592,Rk}/F_{ax,LBA,Rk}\}$ 

Table B.18: Force F<sub>5</sub>, 1 hold-down / connection timber to rigid support

WKR hold down	Fastener pattern	Timber-to-rigid support connection		
		F <sub>5,Rk</sub> [kN]		() []
		LBA nails 4x60 <sup>a</sup>	LBS screws 5x50 b	$$ $\ell_{\rm BL}$ [mm]
WKR9530	1	2,6	3,4	70
WKR13535	1	2,6	3,6	70
WKR21535	1	2,6	3,6	70
WKR28535	1-4	0,9	0,9	160
WKR28535	2	2,6	3,6	70
WKR41035	1	0,43	0,43	278
WKR53035	1	0,33	0,33	343
WKR53035	2	0,26	0,26	423

 $<sup>^</sup>a$  For LBA nails with shorter length,  $F_{5,Rk}$  must be reduced by min{F\_{v,short,Rk}/F\_{v,60,Rk}}; F\_{ax,short,Rk}/F\_{ax,60,Rk}} For ringed shank nails according to EN 14592,  $F_{5,Rk}$  must be reduced by min{F\_{v,EN14592,Rk}/F\_{v,LBA,Rk}}; F\_{ax,EN14592,Rk}/F\_{ax,LBA,Rk}}

The combined action of axial load  $F_{ax,Ed}$  and lateral load  $F_{5,Ed}$  on the fastener in the horizontal flange must be checked by the designer.

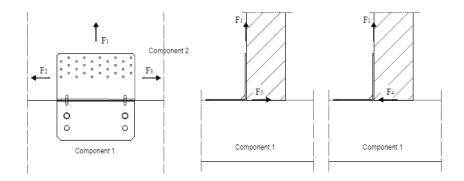
Where:

$$F_{ax,Ed} = \frac{F_{5,Ed} \cdot \ell_{BL}}{25 \text{ mm}}$$
(B.1)

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length,  $F_{5,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

<sup>&</sup>lt;sup>b</sup> For LBS screws with shorter length,  $F_{5,Rk}$  must be reduced by min $\{F_{v,short,Rk}/F_{v,50,Rk}; F_{ax,short,Rk}/F_{ax,50,Rk}\}$ 

## Definitions of forces, their directions and eccentricity Forces – Example:



#### **Fastener specification**

Nailing patterns are given in figures B.8 to B.14, B.20 and B.22.

#### Double angle brackets per connection

The angle brackets must be placed at each side opposite to each other, symmetrically to the component axis. Acting forces

 $F_1$  Lifting force acting along the central axis of the joint.

F<sub>2</sub> and F<sub>3</sub> Lateral force acting in the joint between the component 2 and component 1 in the component 2

direction

 $F_4$  and  $F_5$  Lateral force acting in the component 1 direction along the central axis of the joint.

#### Single angle bracket per connection

Acting forces

F<sub>1</sub> Lifting force acting in the central axis of the angle bracket. The component 2 shall be prevented

from rotation.

F<sub>2</sub> and F<sub>3</sub> Lateral force acting in the joint between the component 2 and the component 1 in the component

2 direction. The component 2 shall be prevented from rotation.

 $F_4$  and  $F_5$  Lateral force acting in the component 1 direction along the central axis of the joint. The compo-

nents must be prevented from rotation. F4 causes compression between the angle bracket or hold-

down and component 2; F<sub>5</sub> causes tension between the angle bracket and component 2.

#### Wane

Wane is not allowed, the timber has to be sharp-edged in the area of the angle brackets.

#### **Timber splitting**

For the lifting force  $F_1$  it must be checked in accordance with Eurocode 5 or a similar national Timber Code that splitting will not occur.

#### **Combined forces**

If the forces  $F_1$  and  $F_2/F_3$  or  $F_4/F_5$  act at the same time, the following inequality shall be fulfilled:

$$\left(\frac{F_{1,\text{Ed}}}{F_{1,\text{Rd}}}\right)^2 + \left(\frac{F_{2,\text{Ed}}}{F_{2,\text{Rd}}}\right)^2 + \left(\frac{F_{3,\text{Ed}}}{F_{3,\text{Rd}}}\right)^2 + \left(\frac{F_{4,\text{Ed}}}{F_{4,\text{Rd}}}\right)^2 + \left(\frac{F_{5,\text{Ed}}}{F_{5,\text{Rd}}}\right)^2 \leq 1$$

The forces  $F_2$  and  $F_3$  or  $F_4$  and  $F_5$  are forces with opposite direction. Therefore, only one force  $F_2$  or  $F_3$ , and  $F_4$  or  $F_5$ , respectively, is able to act simultaneously with  $F_1$ , while the other shall be set to zero.

#### **Rotho Blaas Angle Brackets**

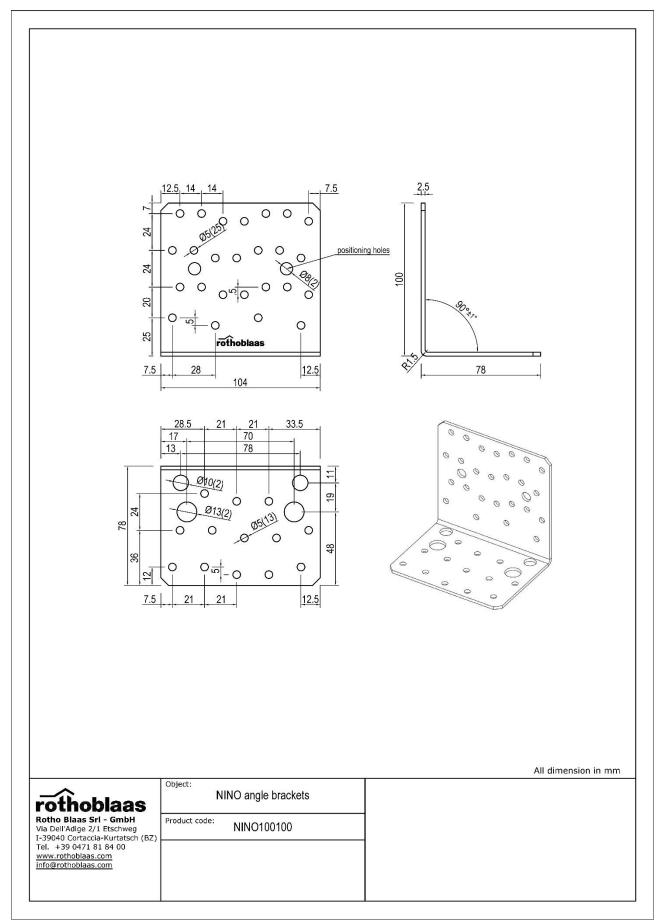


Figure B. 1 Dimensions of Angle Bracket NINO 100100

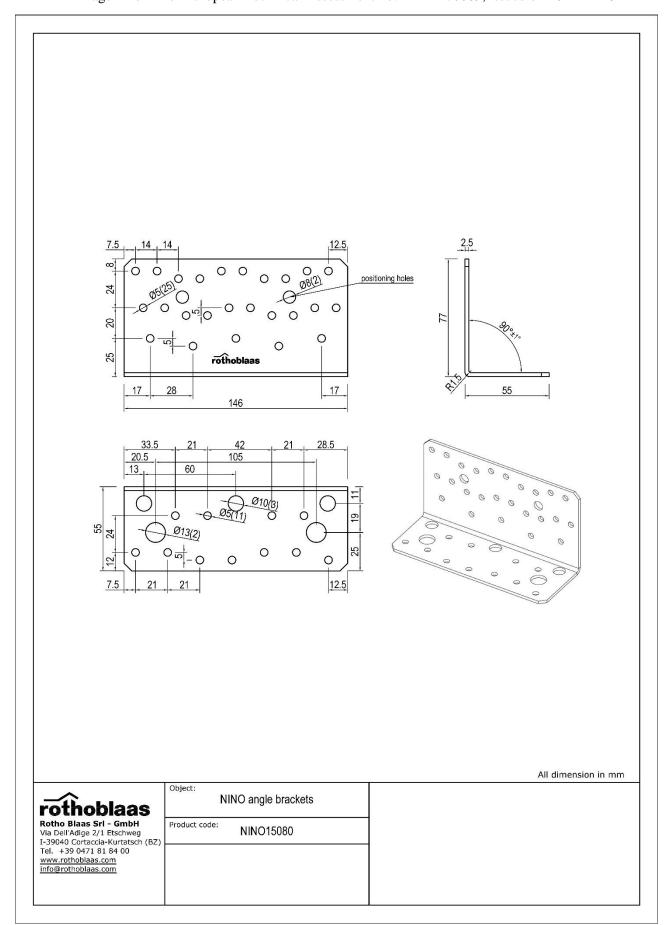


Figure B. 2 Dimensions of Angle Bracket NINO 15080

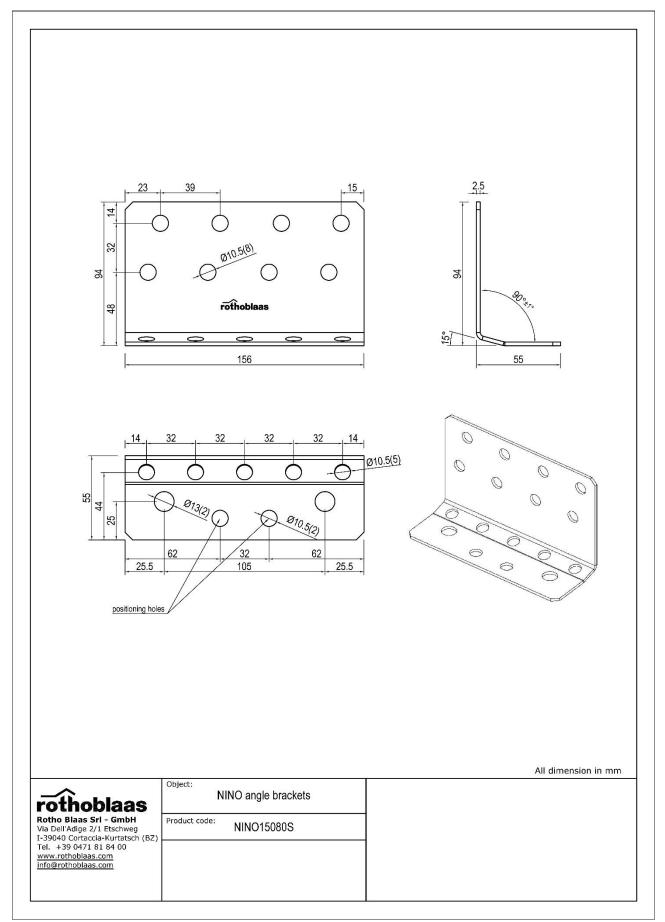


Figure B. 3 Dimensions of Angle Bracket NINO 15080S

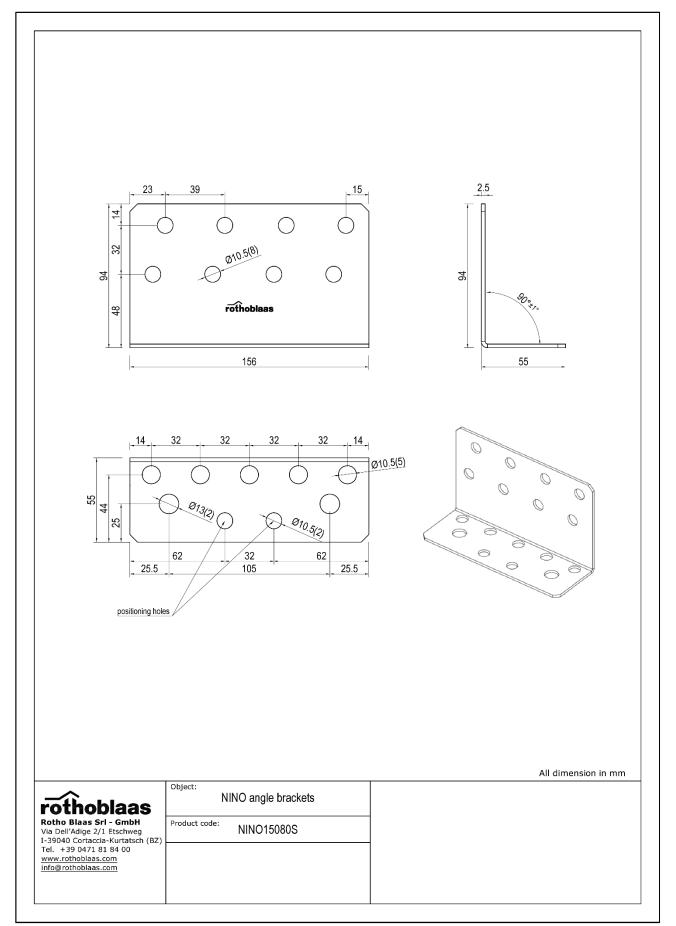


Figure B. 4 Dimensions of Angle Bracket NINO 15080S

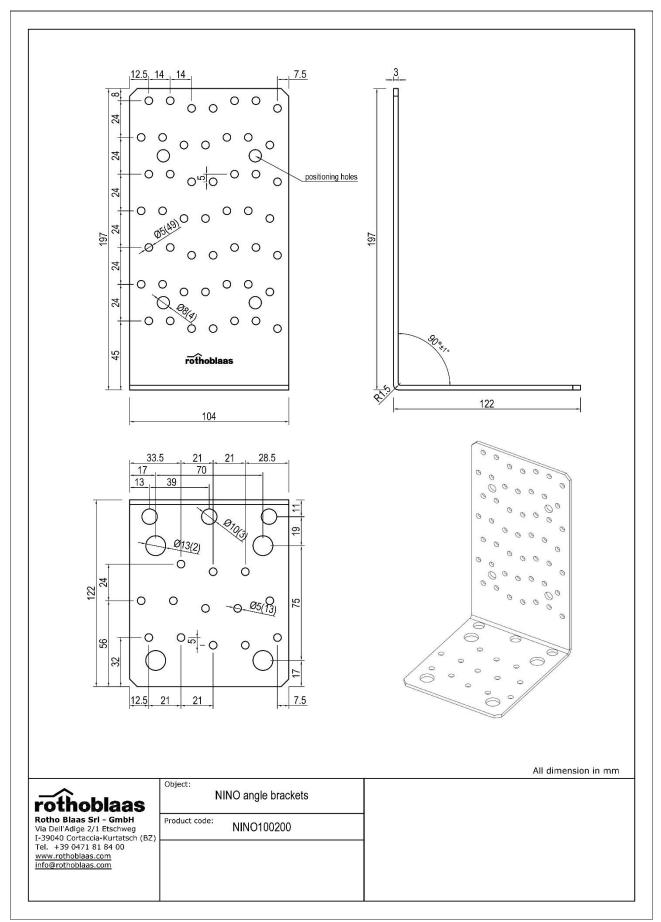


Figure B. 5 Dimensions of Angle Bracket NINO 100200

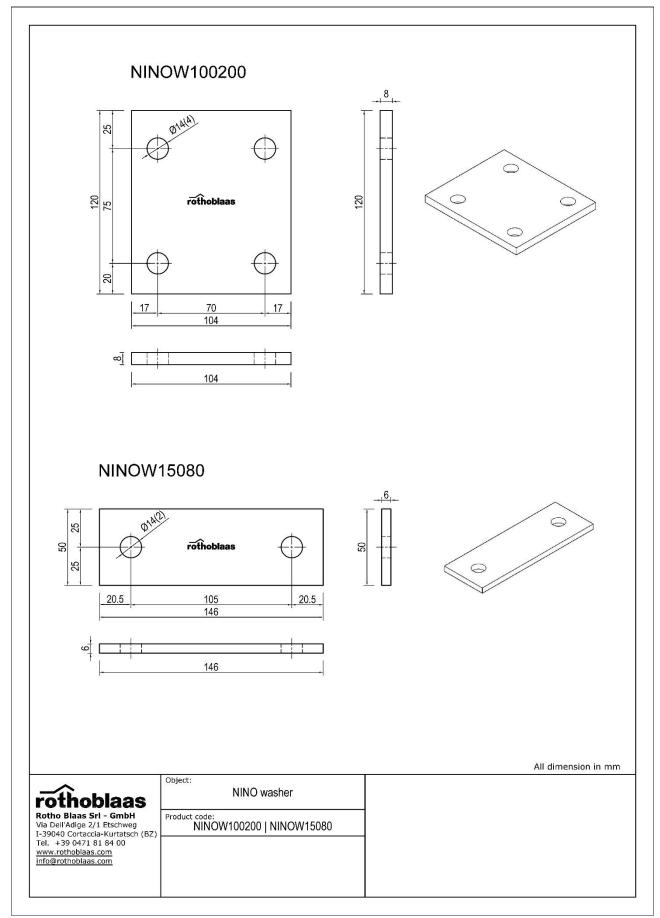


Figure B. 6 Dimensions of NINO Washers



Figure B. 7 Typical installation NINO100100



Figure B. 9 Typical installation NINO15080S

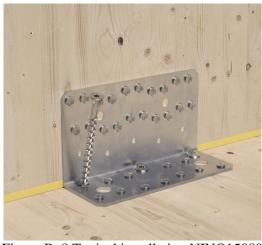


Figure B. 8 Typical installation NINO15080



Figure B. 10 Typical installation NINO100200

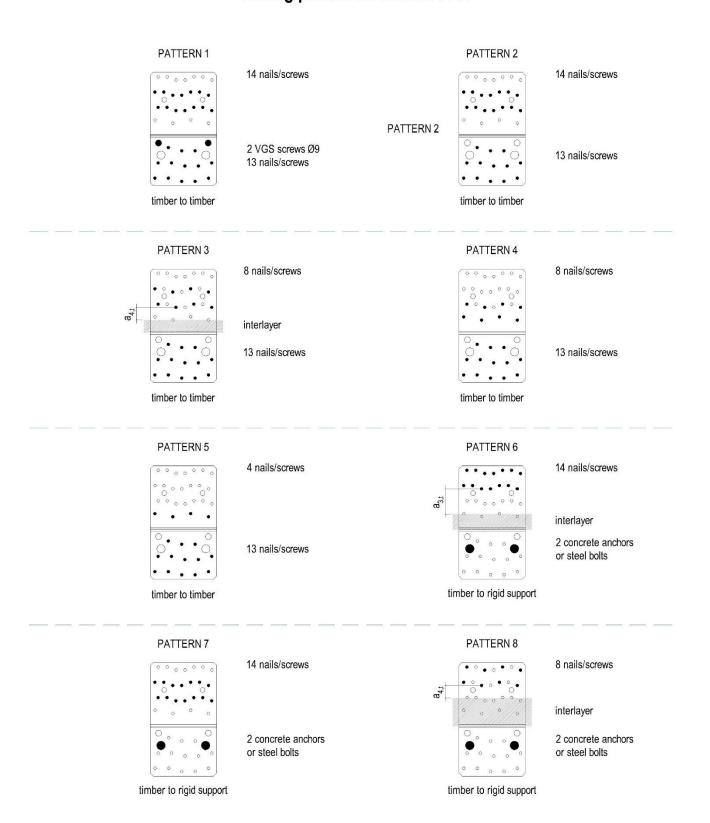


Figure B. 11 Nailing patterns for Angle Bracket NINO 100100

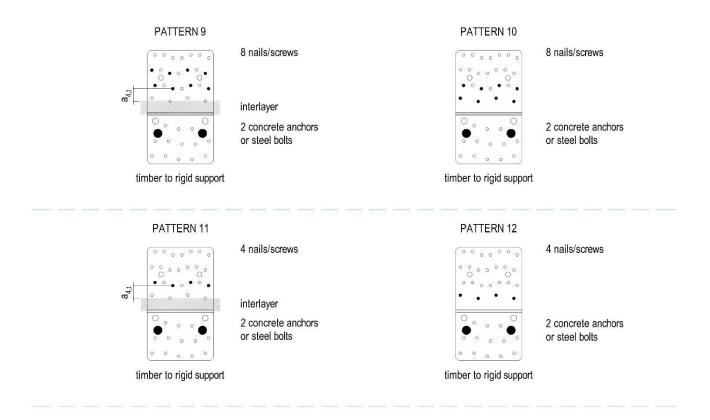


Figure B. 12 Nailing patterns for Angle Bracket NINO 100100

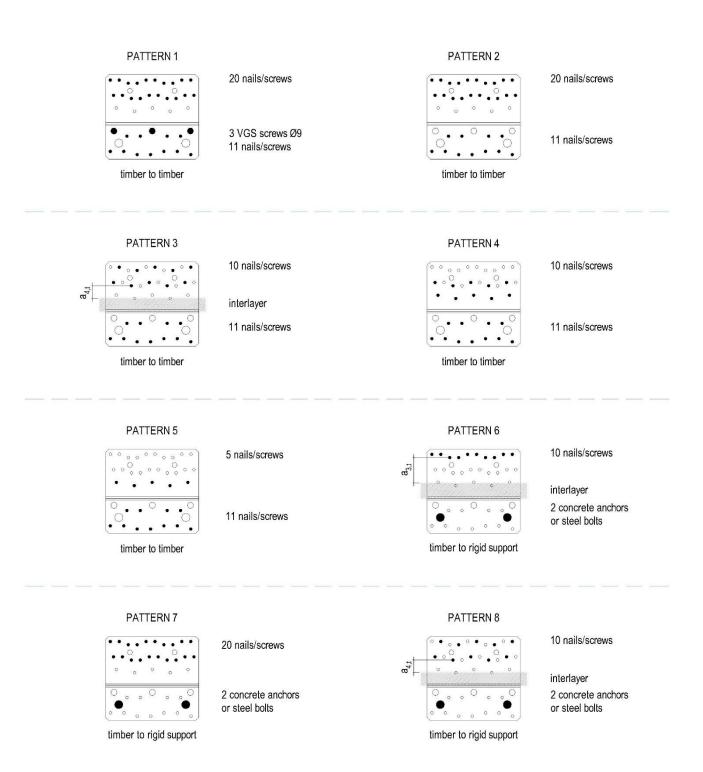


Figure B. 13 Nailing patterns for Angle Bracket NINO 15080

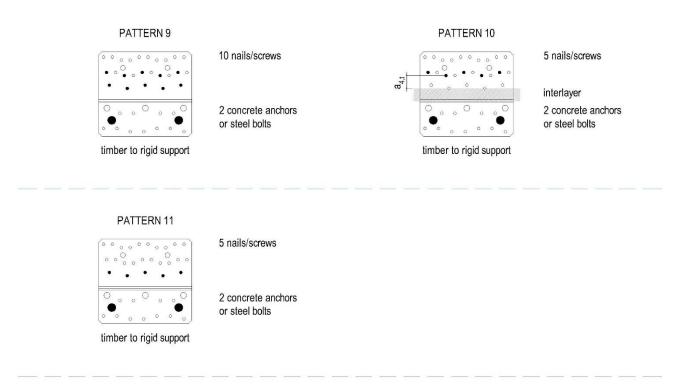


Figure B. 14 Nailing patterns for Angle Bracket NINO 15080

### Nailing pattern for NINO15080S

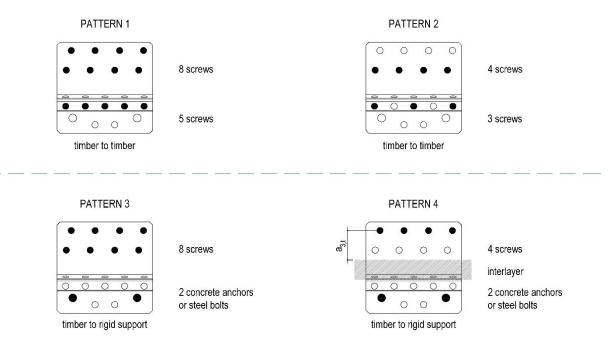
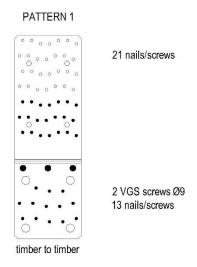


Figure B. 15 Nailing patterns for Angle Bracket NINO 15080S



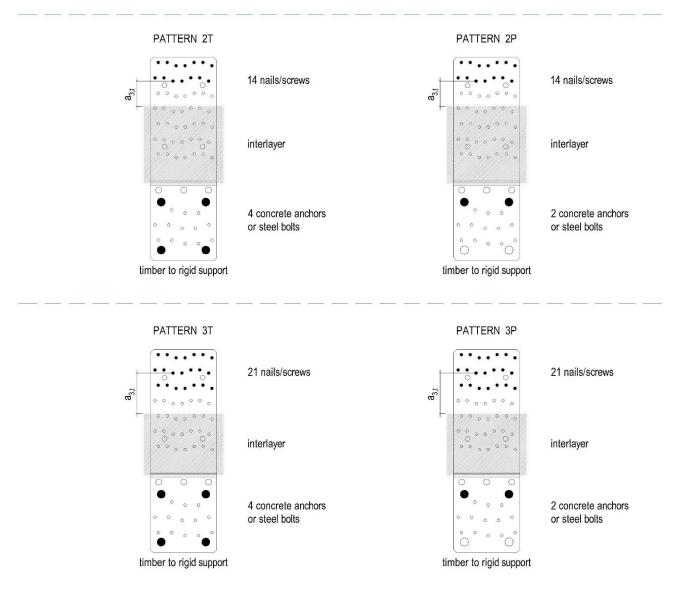


Figure B. 16 Nailing patterns for Angle Bracket NINO 100200

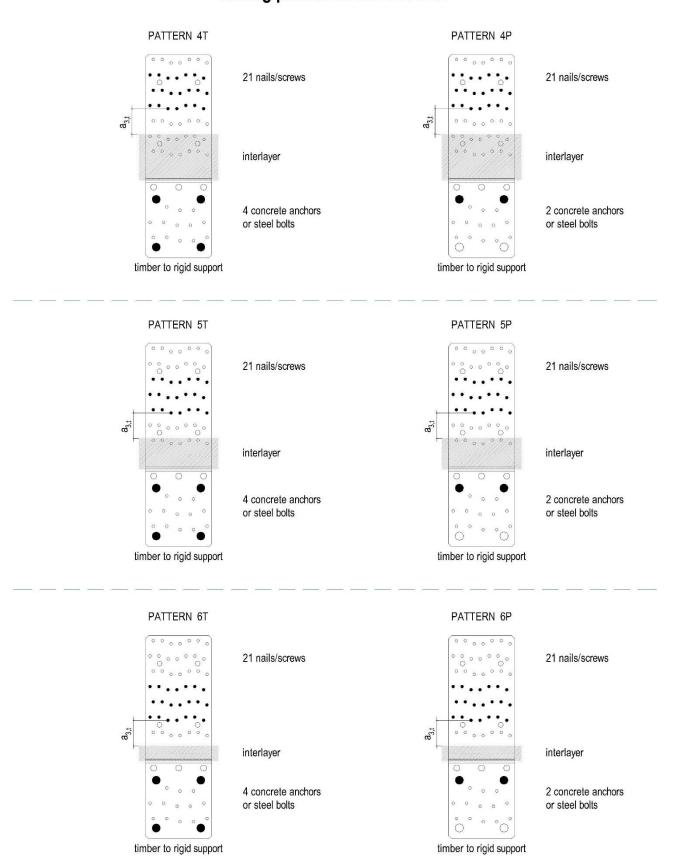


Figure B. 17 Nailing patterns for Angle Bracket NINO 100200

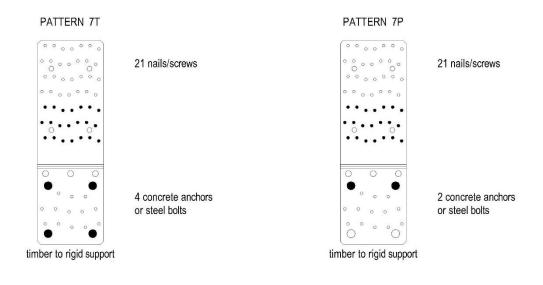


Figure B. 18 Nailing pattern for Angle Bracket NINO 100200

#### **Rotho Blaas Hold-downs**

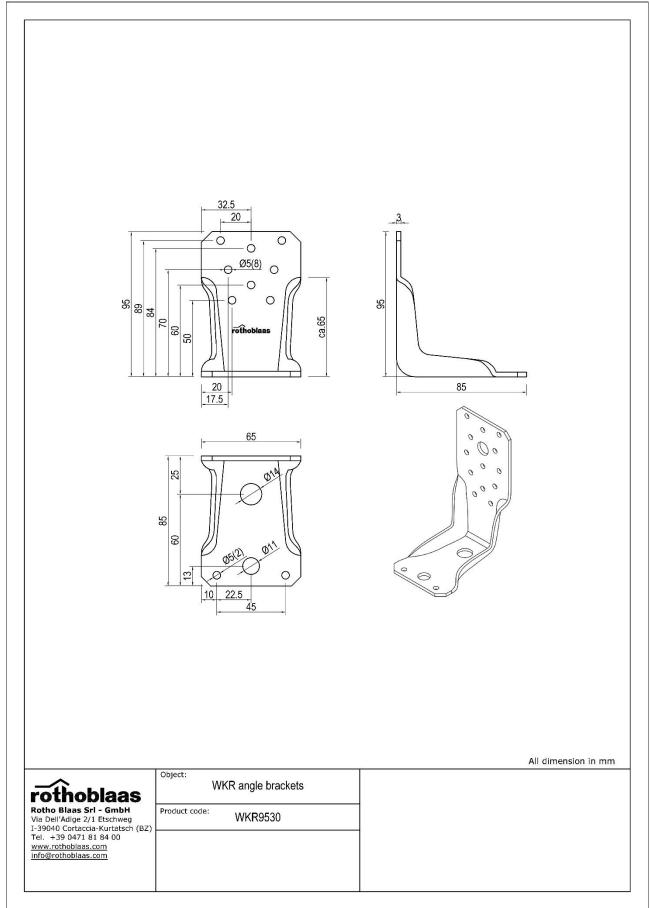


Figure B. 19 Dimensions of Rotho Blaas WKR9530

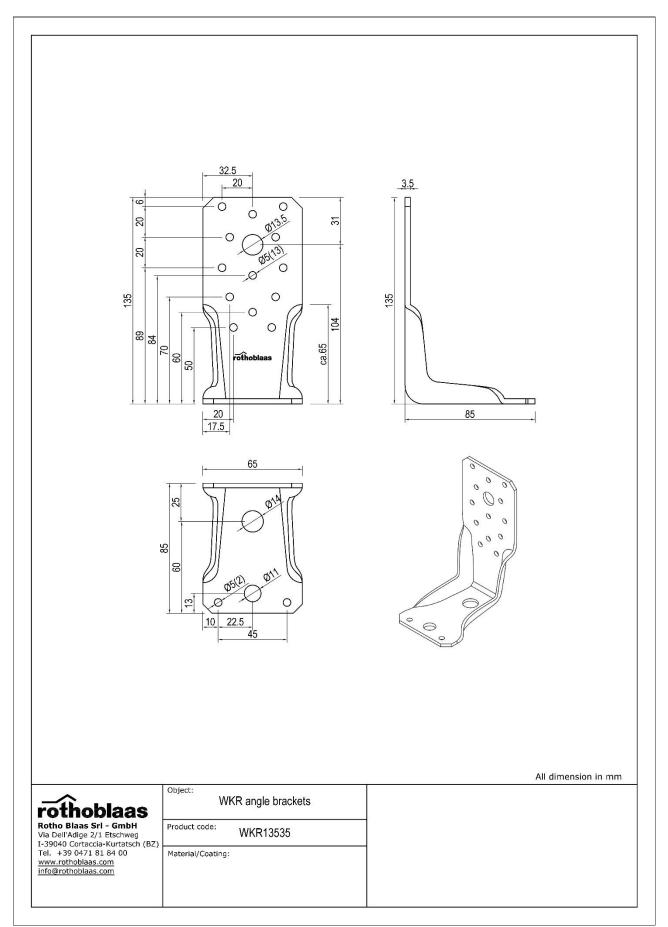


Figure B. 20 Dimensions of Rotho Blaas WKR13535

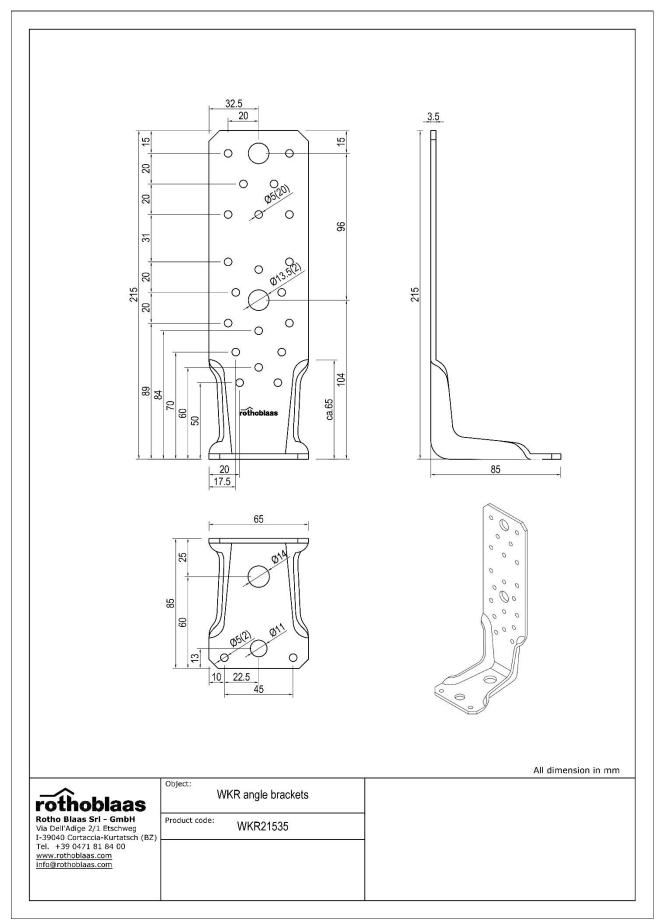


Figure B. 21 Dimensions of Rotho Blaas WKR21535

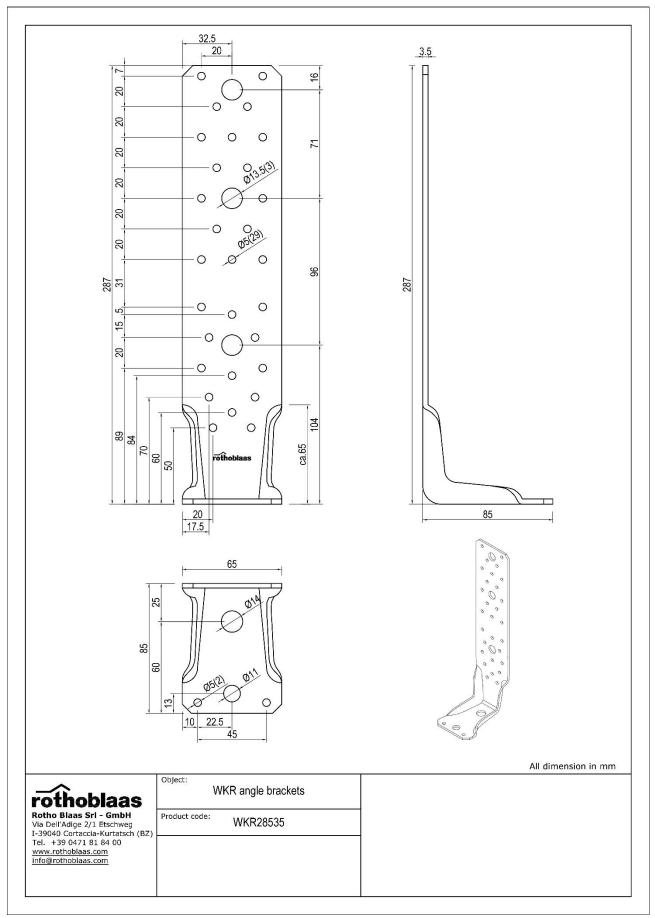


Figure B. 22 Dimensions of Rotho Blaas WKR28535

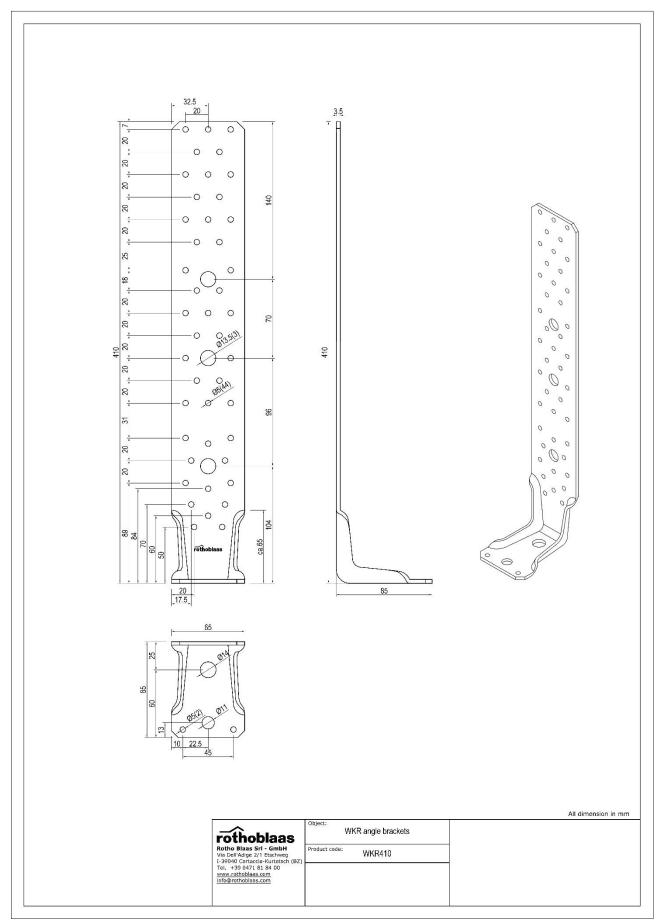


Figure B. 23 Dimensions of Rotho Blaas WKR41035

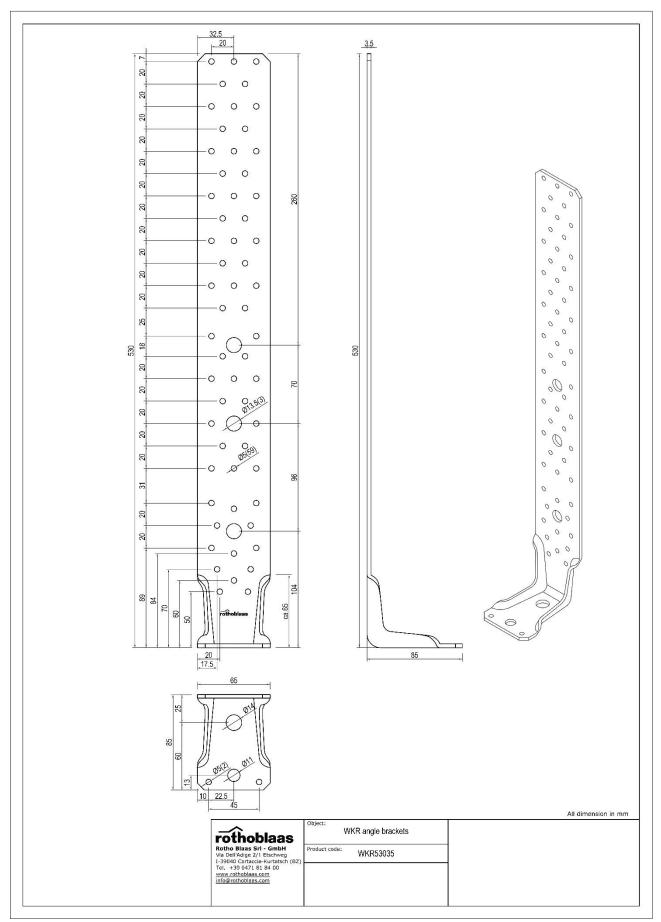


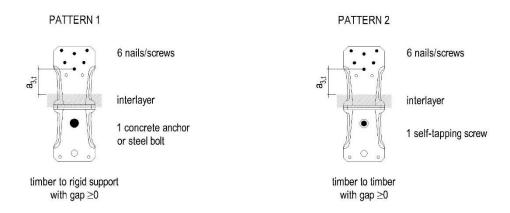
Figure B. 24 Dimensions of Rotho Blaas WKR53035



Figure B. 25 Typical installation WKR135



Figure B. 26 Typical installation WKR285



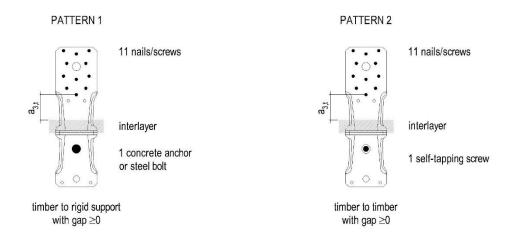


Figure B. 27 Nailing patterns for WKR095 and WKR135

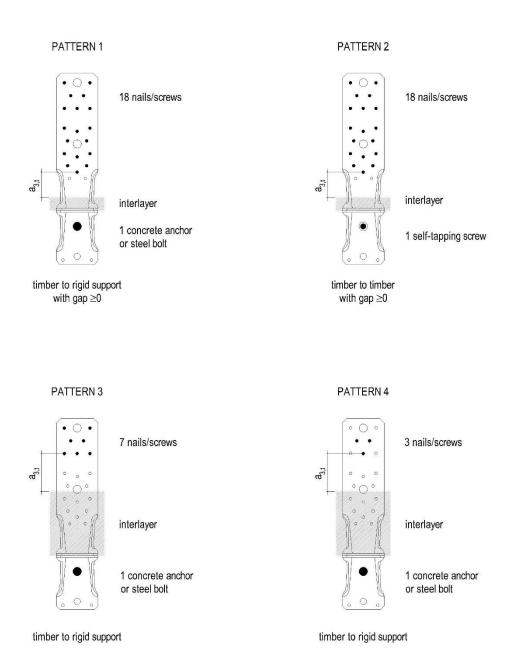
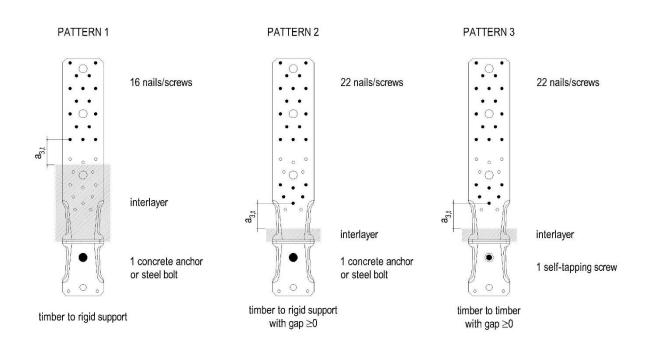


Figure B. 28 Nailing patterns for WKR215



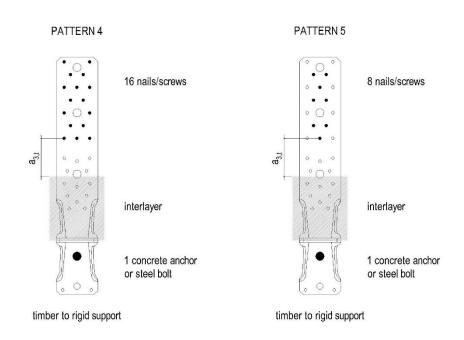
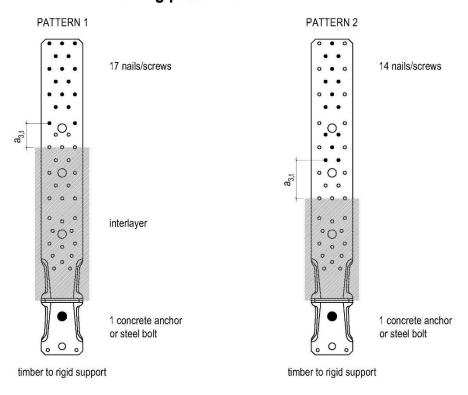


Figure B. 29 Nailing patterns for WKR285



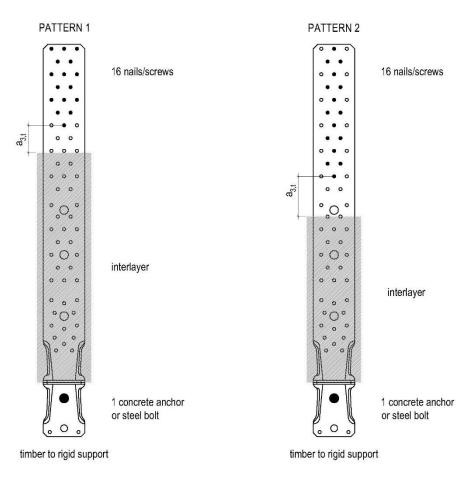


Figure B. 30 Nailing patterns for WKR410 and WKR 530